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On optimization of manufacturing of a bridge rectifier circuit to increase density of elements

EL Pankratov

Abstract

In this paper we introduce an approach to increase density of field-effect transistors in the framework of a bridge rectifier circuit. In the framework of the approach we consider manufacturing the inverter in a heterostructure with specific configuration. Several required areas of the heterostructure should be doped by diffusion or ion implantation. After that dopant and radiation defects should be annealed in the framework of optimized scheme.

Keywords: Bridge rectifier circuit; optimization of manufacturing; analytical approach for prognosis

Introduction

In the present time several actual problems of the solid state electronics (such as increasing of performance, reliability and density of elements of integrated circuits) are intensively solving. At the same time with increasing of density of elements of integrated circuits their dimensions should be decreased. One way to decrease dimensions of these elements is manufacturing integrated circuits in thin films heterostructures ^[1-4]. In this case it could be used inhomogeneity (layering) of heterostructures. An alternative approach to decrease dimensions of elements of integrated circuits using laser or microwave types of annealing ^[5-7]. Using these types of annealing leads to generation inhomogeneous distribution of temperature. In this situation one can find inhomogeneity of diffusion coefficient and another parameters of processes due to Arrhenius law. The inhomogeneity of these parameters gives a possibility to decrease dimensions of elements of integrated circuits. It should be noted, that radiation processing of doped materials also leads to changing their properties ^[8, 9].

In this paper we consider manufacturing of a bridge rectifier circuit ^[10]. Framework the manufacturing we consider a heterostructure, which consist of a substrate and an epitaxial layer. The epitaxial layer includes into itself several sections, which were manufactured by using another materials. These sections have been doped by diffusion or ion implantation to manufacture the required types of conductivity (p or n). These areas became sources, drains and gates (see Fig. 1). After this doping it is required annealing of dopant and/or radiation defects. Main aim of the present paper is analysis of redistribution of dopant and radiation defects to determine conditions, which correspond to decreasing of elements of the considered amplifier and at the same time to increase their density.

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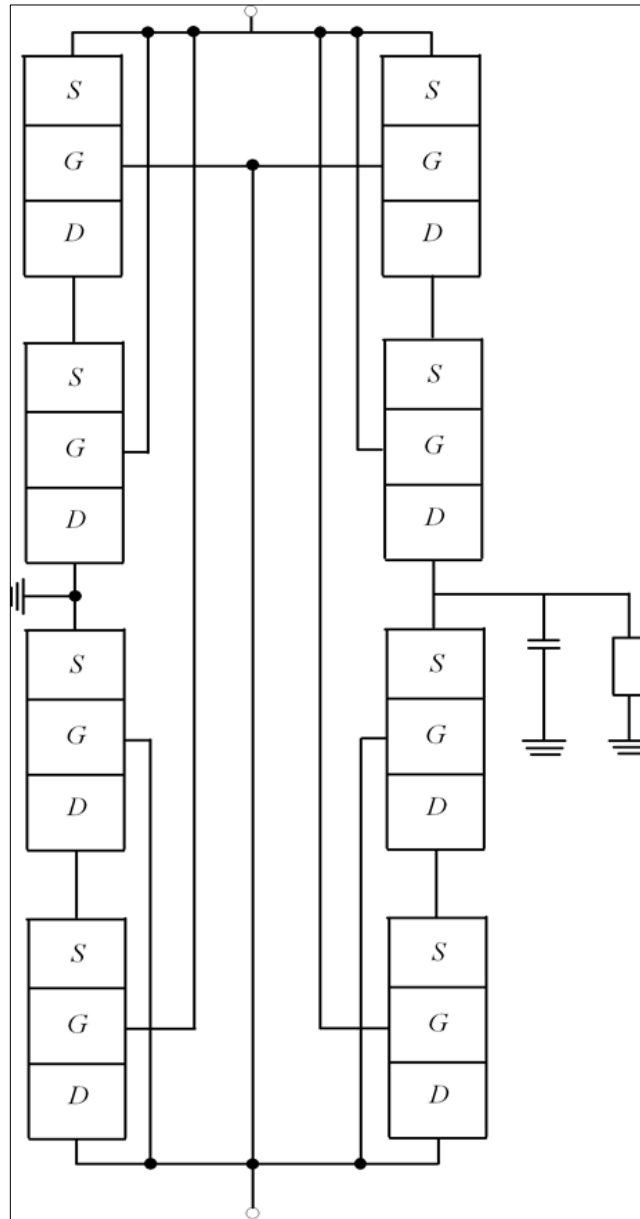


Fig 1: Structure of bridge rectifier circuit. View from top

Method of solution

We determine spatio-temporal distribution of concentration of dopant by solving the following boundary problem

$$\begin{aligned} \frac{\partial C(x,y,z,t)}{\partial t} &= \\ &= \frac{\partial}{\partial \tau^x} \left[D_C \frac{\partial C(x,y,z,t)}{\partial x} \right] + \frac{\partial}{\partial \tau^y} \left[D_C \frac{\partial C(x,y,z,t)}{\partial y} \right] + \frac{\partial}{\partial \tau^z} \left[D_C \frac{\partial C(x,y,z,t)}{\partial z} \right] \end{aligned} \tag{1}$$

with boundary and initial conditions

$$\begin{aligned} \frac{\partial C(x,y,z,t)}{\partial x} \Big|_{x=0} &= 0, \quad \frac{\partial C(x,y,z,t)}{\partial x} \Big|_{x=L_x} = 0, \quad \frac{\partial C(x,y,z,t)}{\partial y} \Big|_{y=0} = 0, \tag{2} \\ \frac{\partial C(x,y,z,t)}{\partial y} \Big|_{x=L_y} &= 0, \quad \frac{\partial C(x,y,z,t)}{\partial z} \Big|_{z=0} = 0, \quad \frac{\partial C(x,y,z,t)}{\partial z} \Big|_{x=L_z} = 0, \quad C(x,y,z,0) = f(x,y,z). \end{aligned}$$

Here $C(x, y, z, t)$ is the spatio-temporal distribution of concentration of dopant; T is the temperature of annealing; D_C is the dopant diffusion coefficient. Value of dopant diffusion coefficient depends on properties of materials, speed of heating and cooling of heterostructure (with account Arrhenius law). Dependences of dopant diffusion coefficients could be approximated by the following function [9, 11, 12].

$$D_C = D_L(x, y, z, T) \left[1 + \xi \frac{C^Y(x,y,z,t)}{P^Y(x,y,z,T)} \right] \left[1 + \zeta_1 \frac{V(x,y,z,t)}{V^*} + \zeta_2 \frac{V^2(x,y,z,t)}{(V^*)^2} \right], \tag{3}$$

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where $D_L(x, y, z, t)$ is the spatial (due to existing several layers with different properties in heterostructure) and temperature (due to Arrhenius law) dependences of dopant diffusion coefficient; $P(x, y, z, t)$ is the limit of solubility of dopant; parameter γ could be integer framework the following interval $\gamma \in [1, 3, 11]$; $V(x, y, z, t)$ is the spatio-temporal distribution of concentration of radiation vacancies; V^* is the equilibrium distribution of concentration of vacancies. Concentration dependence of dopant diffusion coefficient have been discussed in details in [11]. It should be noted, that using diffusion type of doping did not lead to generation radiation defects and $\zeta_1 = \zeta_2 = 0$. We determine spatio-temporal distributions of concentrations of point defects have been determined by solving the following system of equations [9, 12].

$$\begin{aligned} \frac{\partial I(x,y,z,t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_I(x,y,z,T) \frac{\partial I(x,y,z,t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_I(x,y,z,T) \frac{\partial I(x,y,z,t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_I(x,y,z,T) \frac{\partial I(x,y,z,t)}{\partial z} \right] - k_{I,V}(x,y,z,T) I(x,y,z,t) V(x,y,z,t) - \\ &- k_{I,I}(x,y,z,T) I^2(x,y,z,t) \end{aligned} \quad (4)$$

$$\begin{aligned} \frac{\partial V(x,y,z,t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_V(x,y,z,T) \frac{\partial V(x,y,z,t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_V(x,y,z,T) \frac{\partial V(x,y,z,t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_V(x,y,z,T) \frac{\partial V(x,y,z,t)}{\partial z} \right] - k_{I,V}(x,y,z,T) I(x,y,z,t) V(x,y,z,t) - \\ &- k_{V,V}(x,y,z,T) V^2(x,y,z,t) \end{aligned}$$

with boundary and initial conditions

$$\begin{aligned} \left. \frac{\partial \rho(x,y,z,t)}{\partial x} \right|_{x=0} = 0, \quad \left. \frac{\partial \rho(x,y,z,t)}{\partial x} \right|_{x=L_x} = 0, \quad \left. \frac{\partial \rho(x,y,z,t)}{\partial y} \right|_{y=0} = 0, \quad \left. \frac{\partial \rho(x,y,z,t)}{\partial y} \right|_{y=L_y} = 0, \\ \left. \frac{\partial \rho(x,y,z,t)}{\partial z} \right|_{z=0} = 0, \quad \left. \frac{\partial \rho(x,y,z,t)}{\partial z} \right|_{z=L_z} = 0, \quad \rho(x,y,z,0) = f_\rho(x,y,z). \end{aligned} \quad (5)$$

Here $\rho = I, V$; $I(x, y, z, t)$ is the spatio-temporal distribution of concentration of radiation interstitials; $D_\rho(x, y, z, t)$ is the diffusion coefficients of radiation interstitials and vacancies; terms $V^2(x, y, z, t)$ and $I^2(x, y, z, t)$ correspond to generation of divacancies and diinterstitials; $k_{I,V}(x, y, z, t)$ is the parameter of recombination of point radiation defects; $k_{\rho,\rho}(x, y, z, t)$ are the parameters of generation of simplest complexes of point radiation defects.

We determine spatio-temporal distributions of concentrations of divacancies $\Phi_V(x, y, z, t)$ and diinterstitials $\Phi_I(x, y, z, t)$ by solving the following system of equations [11, 12].

$$\begin{aligned} \frac{\partial \Phi_I(x,y,z,t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_{\Phi_I}(x,y,z,T) \frac{\partial \Phi_I(x,y,z,t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_{\Phi_I}(x,y,z,T) \frac{\partial \Phi_I(x,y,z,t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_{\Phi_I}(x,y,z,T) \frac{\partial \Phi_I(x,y,z,t)}{\partial z} \right] + k_{I,I}(x,y,z,T) I^2(x,y,z,t) - k_I(x,y,z,T) I(x,y,z,t) \end{aligned} \quad (6)$$

$$\begin{aligned} \frac{\partial \Phi_V(x,y,z,t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_{\Phi_V}(x,y,z,T) \frac{\partial \Phi_V(x,y,z,t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_{\Phi_V}(x,y,z,T) \frac{\partial \Phi_V(x,y,z,t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_{\Phi_V}(x,y,z,T) \frac{\partial \Phi_V(x,y,z,t)}{\partial z} \right] + k_{V,V}(x,y,z,T) V^2(x,y,z,t) - k_V(x,y,z,T) V(x,y,z,t) \end{aligned}$$

with boundary and initial conditions

$$\begin{aligned} \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial x} \right|_{x=0} = 0, \quad \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial x} \right|_{x=L_x} = 0, \quad \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial y} \right|_{y=0} = 0, \\ \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial y} \right|_{y=L_y} = 0, \quad \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial z} \right|_{z=0} = 0, \quad \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial z} \right|_{z=L_z} = 0, \end{aligned} \quad (7)$$

$$\Phi_I(x, y, z, 0) = f_{\Phi_I}(x, y, z), \quad \Phi_V(x, y, z, 0) = f_{\Phi_V}(x, y, z).$$

Here $D_{\Phi_\rho}(x, y, z, t)$ are the diffusion coefficients of complexes of radiation defects; $k_{\rho,\rho}(x, y, z, t)$ are the parameters of decay of complexes of radiation defects.

We determine spatio-temporal distributions of concentrations of dopant and radiation defects by using method of averaging of function corrections [13] with decreased quantity of iteration steps [14]. Framework the approach we used solutions of Eqs. (1), (4) and (6) in linear form and with averaged values of diffusion coefficients $D_{0L}, D_{0I}, D_{0V}, D_{0\Phi_I}, D_{0\Phi_V}$ as initial-order approximations of the required concentrations. The solutions could be written as

$$C_1(x, y, z, t) = \frac{F_{0C}}{L_x L_y L_z} + \frac{2}{L_x L_y L_z} \sum_{n=1}^{\infty} F_{nC} c_n(x) c_n(y) c_n(z) e_{nC}(t),$$

$$I_1(x, y, z, t) = \frac{F_{0I}}{L_x L_y L_z} + \frac{2}{L_x L_y L_z} \sum_{n=1}^{\infty} F_{nI} c_n(x) c_n(y) c_n(z) e_{nI}(t),$$

$$V_1(x, y, z, t) = \frac{F_{0V}}{L_x L_y L_z} + \frac{2}{L_x L_y L_z} \sum_{n=1}^{\infty} F_{nV} c_n(x) c_n(y) c_n(z) e_{nV}(t),$$

$$\Phi_{I1}(x, y, z, t) = \frac{F_{0\Phi_I}}{L_x L_y L_z} + \frac{2}{L_x L_y L_z} \sum_{n=1}^{\infty} F_{n\Phi_I} c_n(x) c_n(y) c_n(z) e_{n\Phi_I}(t),$$

$$\Phi_{V1}(x, y, z, t) = \frac{F_{0\Phi_V}}{L_x L_y L_z} + \frac{2}{L_x L_y L_z} \sum_{n=1}^{\infty} F_{n\Phi_V} c_n(x) c_n(y) c_n(z) e_{n\Phi_V}(t),$$

where

$$e_{n\rho}(t) = \exp \left[-\pi^2 n^2 D_{0\rho} t \left(\frac{1}{L_x^2} + \frac{1}{L_y^2} + \frac{1}{L_z^2} \right) \right], F_{n\rho} = \int_0^{L_x} c_n(u) \int_0^{L_y} c_n(v) \int_0^{L_z} c_n(w) f_\rho(u, v, w) dw dv du, c_n(\chi) = \cos(\pi n \chi / L_\chi).$$

The second-order approximations and approximations with higher orders of concentrations of dopant and radiation defects determine framework standard iterative procedure [13, 14]. Framework this procedure to calculate approximations with the n -order one shall replace the functions $C(x, y, z, t)$, $I(x, y, z, t)$, $V(x, y, z, t)$, $\Phi_I(x, y, z, t)$, $\Phi_V(x, y, z, t)$ in the right sides of the Eqs. (1), (4) and (6) on the following sums $\alpha_{n\rho} + \rho_{n-1}(x, y, z, t)$. As an example we present equations for the second-order approximations of the considered concentrations

$$\begin{aligned} \frac{\partial C_2(x, y, z, t)}{\partial t} &= \frac{\partial}{\partial x} \left(\left[1 + \zeta_1 \frac{V(x, y, z, t)}{V^*} + \zeta_2 \frac{V^2(x, y, z, t)}{(V^*)^2} \right] \left\{ 1 + \xi \frac{[\alpha_{2C} + C_1(x, y, z, t)]^Y}{P^Y(x, y, z, T)} \right\} \right) \times \\ &\times D_L(x, y, z, T) \frac{\partial C_1(x, y, z, t)}{\partial x} + \frac{\partial}{\partial y} \left(D_L(x, y, z, T) \left[1 + \zeta_1 \frac{V(x, y, z, t)}{V^*} + \zeta_2 \frac{V^2(x, y, z, t)}{(V^*)^2} \right] \right) \times \\ &\times \left\{ 1 + \xi \frac{[\alpha_{2C} + C_1(x, y, z, t)]^Y}{P^Y(x, y, z, T)} \right\} \frac{\partial C_1(x, y, z, t)}{\partial y} + \frac{\partial}{\partial z} \left(D_L(x, y, z, T) \frac{\partial C_1(x, y, z, t)}{\partial z} \right) \times \\ &\times \left[1 + \zeta_1 \frac{V(x, y, z, t)}{V^*} + \zeta_2 \frac{V^2(x, y, z, t)}{(V^*)^2} \right] \left\{ 1 + \xi \frac{[\alpha_{2C} + C_1(x, y, z, t)]^Y}{P^Y(x, y, z, T)} \right\} \end{aligned} \quad (8)$$

$$\begin{aligned} \frac{\partial I_2(x, y, z, t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_I(x, y, z, T) \frac{\partial I_1(x, y, z, t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_I(x, y, z, T) \frac{\partial I_1(x, y, z, t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_I(x, y, z, T) \frac{\partial I_1(x, y, z, t)}{\partial z} \right] - k_{I,V}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, t)] [\alpha_{2V} + V_1(x, y, z, t)] - \\ &- k_{I,I}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, t)]^2 \end{aligned} \quad (9)$$

$$\begin{aligned} \frac{\partial V_2(x, y, z, t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_V(x, y, z, T) \frac{\partial V_1(x, y, z, t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_V(x, y, z, T) \frac{\partial V_1(x, y, z, t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_V(x, y, z, T) \frac{\partial V_1(x, y, z, t)}{\partial z} \right] - k_{I,V}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, t)] [\alpha_{2V} + V_1(x, y, z, t)] - \\ &- k_{V,V}(x, y, z, T) [\alpha_{2V} + V_1(x, y, z, t)]^2 \end{aligned}$$

$$\begin{aligned} \frac{\partial \Phi_{I2}(x, y, z, t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_{\Phi_I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_{\Phi_I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_{\Phi_I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, t)}{\partial z} \right] + k_{I,I}(x, y, z, T) I^2(x, y, z, t) - k_I(x, y, z, T) I(x, y, z, t) \end{aligned} \quad (10)$$

$$\begin{aligned} \frac{\partial \Phi_{V2}(x, y, z, t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_{\Phi_V}(x, y, z, T) \frac{\partial \Phi_{V1}(x, y, z, t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_{\Phi_V}(x, y, z, T) \frac{\partial \Phi_{V1}(x, y, z, t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_{\Phi_V}(x, y, z, T) \frac{\partial \Phi_{V1}(x, y, z, t)}{\partial z} \right] + k_{V,V}(x, y, z, T) V^2(x, y, z, t) - k_V(x, y, z, T) V(x, y, z, t). \end{aligned}$$

Integration of the left and right sides of Eqs.(8)-(10) gives us possibility to obtain relations for the second-order approximations of concentrations of dopant and radiation defects in final form

$$\begin{aligned}
C_2(x, y, z, t) = & \frac{\partial}{\partial \tau x} \left(\int_0^t \left[1 + \zeta_1 \frac{V(x, y, z, \tau)}{V^*} + \zeta_2 \frac{V^2(x, y, z, \tau)}{(V^*)^2} \right] \left\{ 1 + \xi \frac{[\alpha_{2C} + C_1(x, y, z, \tau)]^Y}{P^Y(x, y, z, T)} \right\} \times \right. \\
& \times D_L(x, y, z, T) \frac{\partial C_1(x, y, z, \tau)}{\partial x} \left. \right) d\tau + \frac{\partial}{\partial \tau^2 y} \left(\int_0^t \left[1 + \zeta_1 \frac{V(x, y, z, \tau)}{V^*} + \zeta_2 \frac{V^2(x, y, z, \tau)}{(V^*)^2} \right] \times \right. \\
& \times D_L(x, y, z, T) \left\{ 1 + \xi \frac{[\alpha_{2C} + C_1(x, y, z, \tau)]^Y}{P^Y(x, y, z, T)} \right\} \frac{\partial C_1(x, y, z, \tau)}{\partial y} \left. \right) d\tau + \frac{\partial}{\partial \tau^2 z} \left(\int_0^t D_L(x, y, z, T) \times \right. \\
& \times \left[1 + \zeta_1 \frac{V(x, y, z, \tau)}{V^*} + \zeta_2 \frac{V^2(x, y, z, \tau)}{(V^*)^2} \right] \left\{ 1 + \xi \frac{[\alpha_{2C} + C_1(x, y, z, \tau)]^Y}{P^Y(x, y, z, T)} \right\} \frac{\partial C_1(x, y, z, \tau)}{\partial z} \left. \right) d\tau + \\
& + f_C(x, y, z)
\end{aligned} \tag{8a}$$

$$\begin{aligned}
I_2(x, y, z, t) = & \frac{\partial}{\partial x} \left[\int_0^t D_I(x, y, z, T) \frac{\partial I_1(x, y, z, \tau)}{\partial x} d\tau \right] + \frac{\partial}{\partial y} \left[\int_0^t D_I(x, y, z, T) \times \right. \\
& \times \frac{\partial I_1(x, y, z, \tau)}{\partial y} d\tau \left. \right] + \frac{\partial}{\partial z} \left[\int_0^t D_I(x, y, z, T) \frac{\partial I_1(x, y, z, \tau)}{\partial z} d\tau \right] - \int_0^t k_{I,I}(x, y, z, T) \times \\
& \times [\alpha_{2I} + I_1(x, y, z, \tau)]^2 d\tau + f_I(x, y, z) - \int_0^t k_{I,V}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, \tau)] \times \\
& \times [\alpha_{2V} + V_1(x, y, z, \tau)] d\tau \tag{9a}
\end{aligned}$$

$$\begin{aligned}
V_2(x, y, z, t) = & \frac{\partial}{\partial x} \left[\int_0^t D_V(x, y, z, T) \frac{\partial V_1(x, y, z, \tau)}{\partial x} d\tau \right] + \frac{\partial}{\partial y} \left[\int_0^t D_V(x, y, z, T) \times \right. \\
& \times \frac{\partial V_1(x, y, z, \tau)}{\partial y} d\tau \left. \right] + \frac{\partial}{\partial z} \left[\int_0^t D_V(x, y, z, T) \frac{\partial V_1(x, y, z, \tau)}{\partial z} d\tau \right] - \int_0^t k_{V,V}(x, y, z, T) \times \\
& \times [\alpha_{2I} + V_1(x, y, z, \tau)]^2 d\tau + f_V(x, y, z) - \int_0^t k_{I,V}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, \tau)] \times \\
& \times [\alpha_{2V} + V_1(x, y, z, \tau)] d\tau
\end{aligned}$$

$$\begin{aligned}
\Phi_{I2}(x, y, z, t) = & \frac{\partial}{\partial x} \left[\int_0^t D_{\Phi_I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, \tau)}{\partial x} d\tau \right] + \frac{\partial}{\partial y} \left[\int_0^t D_{\Phi_I}(x, y, z, T) \times \right. \\
& \times \frac{\partial \Phi_{I1}(x, y, z, \tau)}{\partial y} d\tau \left. \right] + \frac{\partial}{\partial z} \left[\int_0^t D_{\Phi_I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, \tau)}{\partial z} d\tau \right] + \int_0^t k_{I,I}(x, y, z, T) \times \\
& \times I^2(x, y, z, \tau) d\tau - \int_0^t k_I(x, y, z, T) I(x, y, z, \tau) d\tau + f_{\Phi_I}(x, y, z) \tag{10a}
\end{aligned}$$

$$\begin{aligned}
\Phi_{V2}(x, y, z, t) = & \frac{\partial}{\partial x} \left[\int_0^t D_{\Phi_V}(x, y, z, T) \frac{\partial \Phi_{V1}(x, y, z, \tau)}{\partial x} d\tau \right] + \frac{\partial}{\partial y} \left[\int_0^t D_{\Phi_V}(x, y, z, T) \times \right. \\
& \times \frac{\partial \Phi_{V1}(x, y, z, \tau)}{\partial y} d\tau \left. \right] + \frac{\partial}{\partial z} \left[\int_0^t D_{\Phi_V}(x, y, z, T) \frac{\partial \Phi_{V1}(x, y, z, \tau)}{\partial z} d\tau \right] + \int_0^t k_{V,V}(x, y, z, T) \times \\
& \times V^2(x, y, z, \tau) d\tau - \int_0^t k_V(x, y, z, T) V(x, y, z, \tau) d\tau + f_{\Phi_V}(x, y, z)
\end{aligned}$$

We determine average values of the second-orders approximations of the considered concentrations by using the following standard relations ^[13, 14].

$$\alpha_{2\rho} = \frac{1}{\Theta_{L_x L_y L_z}} \int_0^{\Theta} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} [\rho_2(x, y, z, t) - \rho_1(x, y, z, t)] dz dy dx dt. \tag{11}$$

Substitution of relations (8a)-(10a) into relation (11) gives us possibility to obtain relations for the required average values $\alpha_{2\rho}$

$$\alpha_{2C} = \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_C(x, y, z) dz dy dx, \tag{12}$$

$$\begin{aligned}
\alpha_{2I} = & \frac{1}{2A_{II00}} \{ (1 + A_{IV01} + A_{II10} + \alpha_{2V} A_{IV00})^2 - 4A_{II00} [\alpha_{2V} A_{IV10} - A_{II20} + A_{IV11} - \\
& - \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_I(x, y, z) dz dy dx] \}^{\frac{1}{2}} - \frac{1 + A_{IV01} + A_{II10} + \alpha_{2V} A_{IV00}}{2A_{II00}} \tag{13a}
\end{aligned}$$

$$\alpha_{2V} = \frac{1}{2B_4} \sqrt{\frac{(B_3+A)^2}{4} - 4B_4 \left(y + \frac{B_3 y - B_1}{A} \right) - \frac{B_3+A}{4B_4}}, \quad (13b)$$

Where

$$A_{abij} = \frac{1}{\theta L_x L_y L_z} \int_0^\theta (\theta - t) \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} k_{a,b}(x, y, z, T) I_1^i(x, y, z, t) V_1^j(x, y, z, t) dz dy dx dt,$$

$$\begin{aligned} B_4 &= A_{IV00}^2 A_{IV00}^2 - 2(A_{IV00}^2 - A_{II00} A_{VV00})^2, B_3 = A_{IV00} A_{IV00}^2 + A_{IV01} A_{IV00}^3 + A_{IV00} A_{II10} A_{IV00}^2 - \\ &- 4(A_{IV00}^2 - A_{II00} A_{VV00}) [2A_{IV01} A_{IV00} + 2A_{IV00} (1 + A_{IV01} + A_{II10}) - 2A_{II00} (A_{IV10} + A_{VV10} + 1)] - \\ &- 4A_{IV10} A_{II00} A_{IV00}^2 + 2A_{IV00} A_{IV01} A_{IV00}^2, B_2 = A_{IV00}^2 \{ (1 + A_{IV01} + A_{II10})^2 + A_{IV00}^2 A_{IV01}^2 + A_{IV00} \times \\ &\times 2A_{IV00} (A_{IV00} + A_{IV00} A_{IV01} + A_{IV00} A_{II10} - 4A_{IV10} A_{II00}) - 4A_{II00} \left[A_{IV11} - A_{II20} - \frac{1}{L_x L_y L_z} \times \right. \\ &\times \left. \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_I(x, y, z) dz dy dx \right] \} \{ [2A_{IV01} A_{IV00} + 2A_{IV00} (1 + A_{IV01} + A_{II10}) - 2A_{II00} (A_{IV10} + 1 + \\ &+ A_{VV10})]^2 + 2 \left[A_{IV01} (1 + A_{IV01} + A_{II10}) + \frac{2}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_V(x, y, z) dz dy dx - 2A_{II00} (A_{VV20} - \right. \\ &- A_{IV11}) + A_{IV01} (1 + A_{IV01} + A_{II10}) \} [2A_{IV00} (1 + A_{IV01} + A_{II10}) + 2A_{IV01} A_{IV00} - 2A_{II00} (A_{IV10} + 1 + \\ &+ A_{VV10}) \} \}, B_1 = 2A_{IV00} A_{IV01} (1 + A_{IV01} + A_{II10})^2 - 8 \left[A_{IV11} - \frac{1}{L_x} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_I(x, y, z) dz dy dx \times \right. \\ &\times \left. \frac{1}{L_y L_z} - A_{II20} \right] + A_{IV00} A_{IV01} A_{II00} + A_{IV01}^2 (A_{IV00} + A_{IV00} A_{IV01} + A_{IV00} A_{II10} - 4A_{IV10} A_{II00}) - \\ &- 2 \left[\frac{2A_{II00}}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_I(x, y, z) dz dy dx + A_{IV01} (1 + A_{IV01} + A_{II10}) - 2A_{II00} (A_{VV20} - A_{IV11}) + \right. \\ &+ A_{IV01} (1 + A_{IV01} + A_{II10}) \} [2A_{IV00} (1 + A_{IV01} + A_{II10}) - 2(A_{IV10} + A_{VV10} + 1) A_{II00} + 2A_{IV01} A_{IV00}], \\ B_0 &= 4A_{II00} A_{IV01}^2 \left[A_{II20} + \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_I(x, y, z) dz dy dx - A_{IV11} \right] + A_{IV01}^2 (A_{IV01} + A_{II10} + \\ &+ 1)^2 - \left[\frac{2A_{II00}}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_V(x, y, z) dz dy dx + A_{IV01} (1 + A_{IV01} + A_{II10}) - 2A_{II00} (A_{VV20} - A_{IV11}) + \right. \\ &+ A_{IV01} (1 + A_{IV01} + A_{II10}) \}]^2, y = \sqrt[3]{\sqrt{q^2 + p^3} - q} - \sqrt[3]{\sqrt{q^2 + p^3} + q} + \frac{B_2}{6}, q = (2B_1 B_3 - 8B_0) \times \\ &\times \frac{B_2}{48} + \frac{B_2^3}{216} + \frac{B_0(4B_2 - B_3^2) - B_1^2}{8}, p = [3(2B_1 B_3 - 8B_0) - 2B_2^2] / 72, A = \sqrt{8y + B_3^2 - 4B_2}, \\ \alpha_{2\Phi_I} &= A_{II20} - \frac{1}{\theta L_x L_y L_z} \int_0^\theta (\theta - t) \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} k_I(x, y, z, T) I(x, y, z, t) dz dy dx dt + \\ &+ \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_{\Phi_I}(x, y, z) dz dy dx \quad (14) \\ \alpha_{2\Phi_V} &= A_{VV20} - \frac{1}{\theta L_x L_y L_z} \int_0^\theta (\theta - t) \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} k_V(x, y, z, T) V(x, y, z, t) dz dy dx dt + \\ &+ \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_{\Phi_V}(x, y, z) dz dy dx. \end{aligned}$$

The considered substitution gives us possibility to obtain equation for parameter α_{2C} . Solution of the equation depends on value of parameter γ . Analysis of spatio-temporal distributions of concentrations of dopant and radiation defects has been done by using their second-order approximations framework the method of averaged of function corrections with decreased quantity of iterative steps. The second-order approximation is usually enough good approximation to make qualitative analysis and obtain some quantitative results. Results of analytical calculation have been checked by comparison with results of numerical simulation.

Discussion

In this section we analyzed spatio-temporal distribution of concentration of infused (see Fig. 2a) and implanted (see Fig. 2b) dopants in the considered epitaxial layer. Annealing time is the same for the each curve framework each figure. Increasing of number of curve corresponds to increasing of difference between values of dopant diffusion coefficient in layers of heterostructure. The figures show, that interface between layers of heterostructure gives a possibility to increase absolute value of gradient of concentration of dopant in direction, which is perpendicular to the interface. In this situation one can find decreasing of dimensions of transistors framework the considered hybrid cascaded multilevel inverter. At the same time with increasing of absolute value of the above gradient one can find increasing homogeneity of distribution of concentrations of dopants in doped areas.

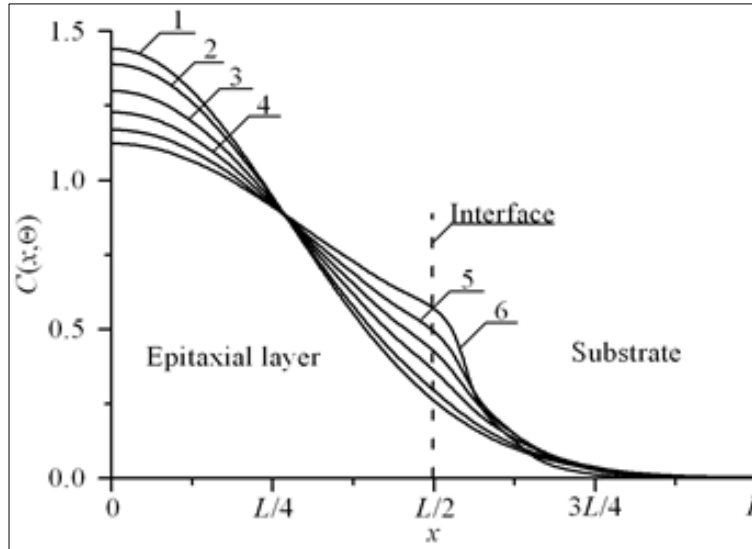


Fig 2a: Distributions of concentration of infused dopant in heterostructure from Figs. 1 and 2 in direction, which is perpendicular to interface between epitaxial layer substrate. Increasing of number of curve corresponds to increasing of difference between values of dopant diffusion coefficient in layers of heterostructure under condition, when value of dopant diffusion coefficient in epitaxial layer is larger, than value of dopant diffusion coefficient in substrate

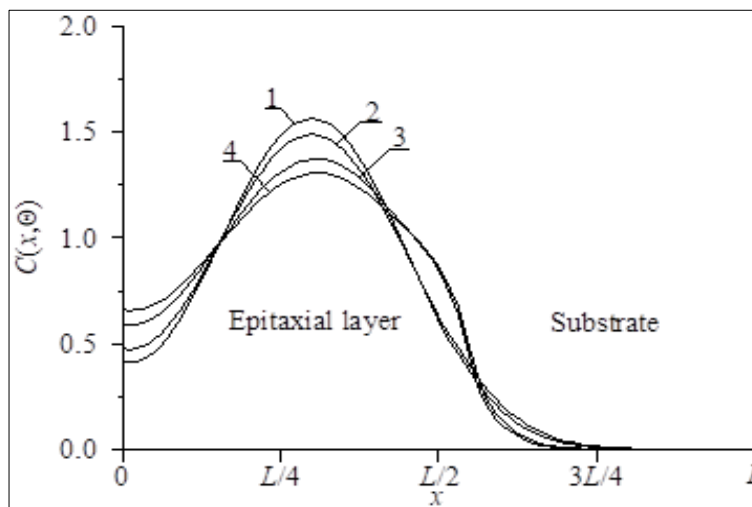


Fig 2b: Distributions of concentration of implanted dopant in heterostructure from Figs. 1 and 2 in direction, which is perpendicular to interface between epitaxial layer substrate. Curves 1 and 3 corresponds to annealing time $\Theta = 0.0048(L_x^2+L_y^2+L_z^2)/D_0$. Curves 2 and 4 corresponds to annealing time $\Theta = 0.0057(L_x^2+L_y^2+L_z^2)/D_0$. Curves 1 and 2 corresponds to homogenous sample. Curves 3 and 4 corresponds to heterostructure under condition, when value of dopant diffusion coefficient in epitaxial layer is larger, than value of dopant diffusion coefficient in substrate

To choose annealing time it is necessary to take into account decreasing of absolute value of gradient of concentration of dopant near interface between epitaxial layer and substrate with increasing of value of annealing time. Decreasing of value of annealing time leads to increasing of inhomogeneity of distribution of concentration of dopant (see Figs. 3a for diffusion type of doping and 3b for ion type of doping). We determine the compromise value of annealing time framework recently introduced criterion^[15-22]. Framework the criterion we approximate real distribution of concentration of dopant by idealized step-wise function $\psi(x, y, z)$. After that we determine the required compromise value of annealing time by minimization of the mean-squared error

$$U = \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} [C(x, y, z, \Theta) - \psi(x, y, z)] dz dy dx. \tag{8}$$

Dependences of optimal annealing time are presented on Figs. 4 for diffusion and ion types of doping, respectively. It should be noted, that it is necessary to anneal radiation defects after ion implantation. One could find spreading of concentration of distribution of dopant during this annealing. In the ideal case distribution of dopant achieves appropriate interfaces between materials of heterostructure during annealing of radiation defects. If dopant did not achieves any interfaces during annealing of radiation defects, it is practicably to additionally anneal the dopant. In this situation optimal value of additional annealing time of implanted dopant is smaller, than annealing time of infused dopant. At the same time ion type of doping gives us possibility to decrease mismatch-induced stress in heterostructure [23].

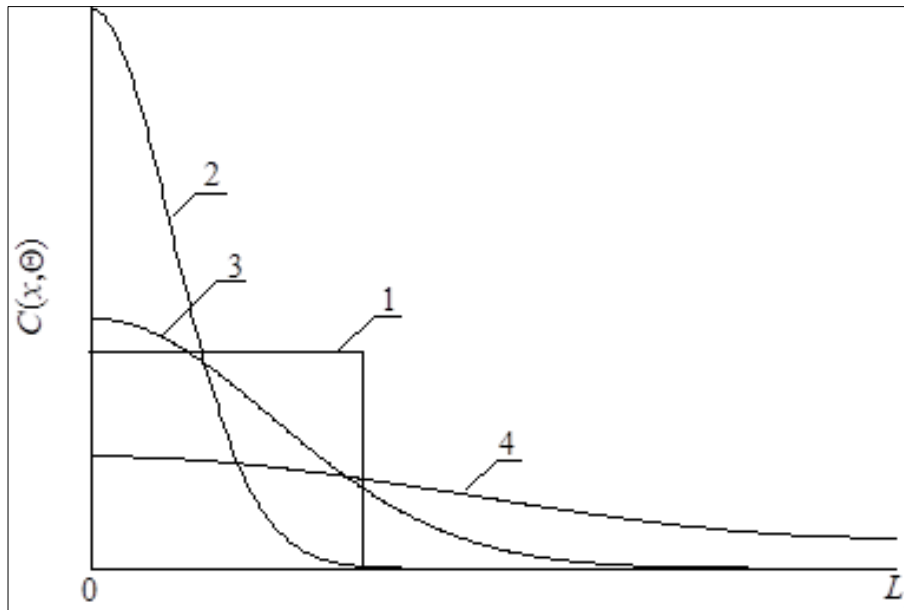


Fig 3a: Spatial distributions of dopant in heterostructure after dopant infusion. Curve 1 is idealized distribution of dopant. Curves 2-4 are real distributions of dopant for different values of annealing time. Increasing of number of curve corresponds to increasing of annealing time

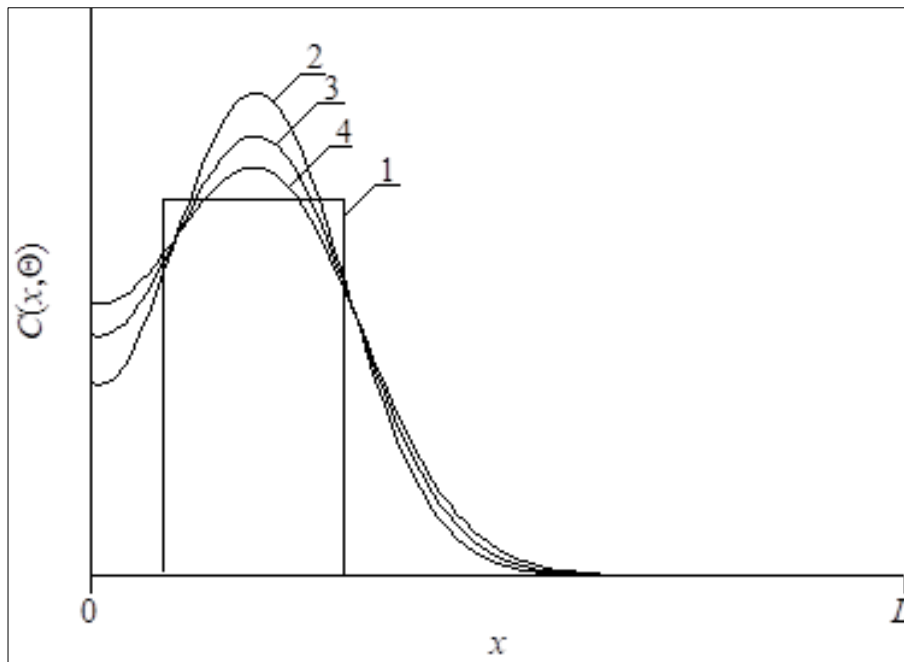


Fig 3b: Spatial distributions of dopant in heterostructure after ion implantation. Curve 1 is idealized distribution of dopant. Curves 2-4 are real distributions of dopant for different values of annealing time. Increasing of number of curve corresponds to increasing of annealing time

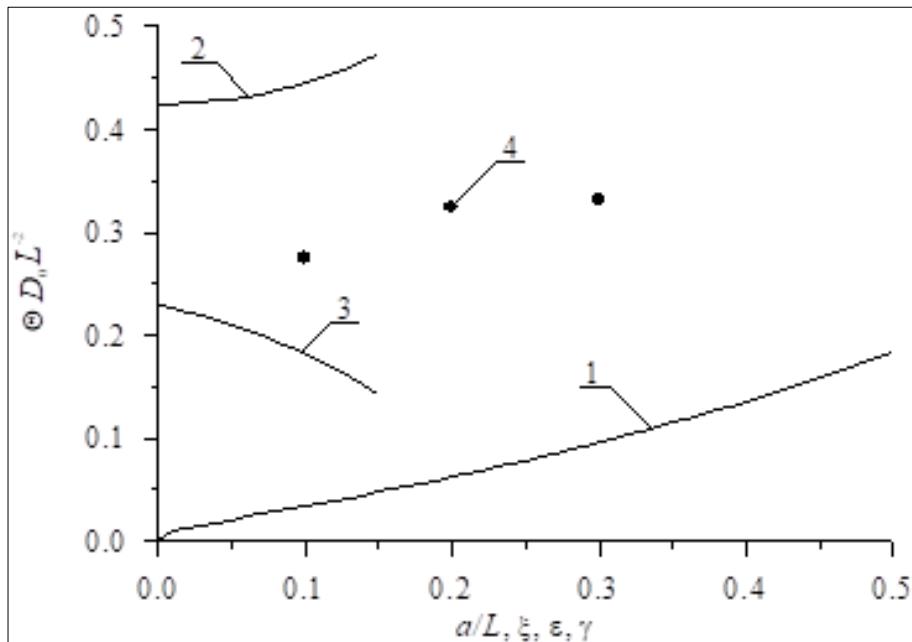


Fig 4a: Dependences of dimensionless optimal annealing time for doping by diffusion, which have been obtained by minimization of mean-squared error, on several parameters. Curve 1 is the dependence of dimensionless optimal annealing time on the relation a/L and $\xi = \gamma = 0$ for equal to each other values of dopant diffusion coefficient in all parts of heterostructure. Curve 2 is the dependence of dimensionless optimal annealing time on value of parameter ε for $a/L=1/2$ and $\xi = \gamma = 0$. Curve 3 is the dependence of dimensionless optimal annealing time on value of parameter ξ for $a/L=1/2$ and $\varepsilon = \gamma = 0$. Curve 4 is the dependence of dimensionless optimal annealing time on value of parameter γ for $a/L=1/2$ and $\varepsilon = \xi = 0$

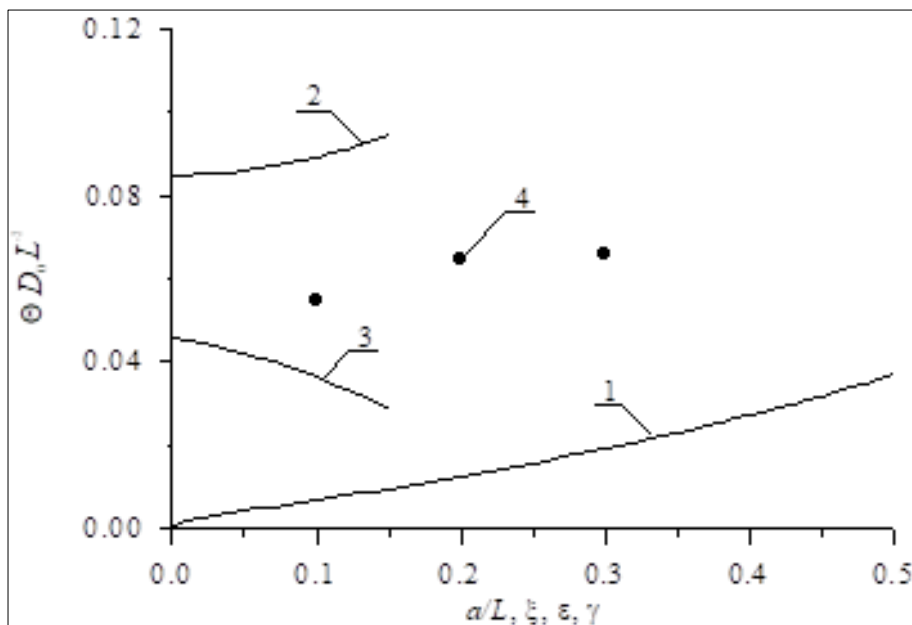


Fig 4b: Dependences of dimensionless optimal annealing time for doping by ion implantation, which have been obtained by minimization of mean-squared error, on several parameters. Curve 1 is the dependence of dimensionless optimal annealing time on the relation a/L and $\xi = \gamma = 0$ for equal to each other values of dopant diffusion coefficient in all parts of heterostructure. Curve 2 is the dependence of dimensionless optimal annealing time on value of parameter ε for $a/L=1/2$ and $\xi = \gamma = 0$. Curve 3 is the dependence of dimensionless optimal annealing time on value of parameter ξ for $a/L=1/2$ and $\varepsilon = \gamma = 0$. Curve 4 is the dependence of dimensionless optimal annealing time on value of parameter γ for $a/L=1/2$ and $\varepsilon = \xi = 0$

Conclusion

In this paper we model redistribution of infused and implanted dopants during manufacturing field-effect heterotransistors framework a bridge rectifier circuit. We formulate recommendations for optimization of annealing to decrease dimensions of transistors and to increase their density. Analytical approach to model diffusion and ion types of doping with account concurrent changing of parameters in space and time has been introduced. At the same time the approach gives us possibility to take into account nonlinearity of considered processes.

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