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# Construction of acceptance sampling plans for the median ranked set sampling using logistic distribution 

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#### Abstract

In this article Single Sampling Plan dependent on Median Ranked data plot is proposed. Two fundamental prerequisites are considered for the new arrangement: the lifetime of the test units is accepted to follow the summed up remarkable circulation; and the information are chosen by utilizing the Median Ranked Set inspecting plan from an enormous part. The appropriation work portrayal under the Median Ranked Set inspecting plan is determined expecting that the set size is known; the base number of set cycle and subsequently the base sample size is important to guarantee the predefined normal life are acquired and the working trademark upsides of the positioned examining plans just as the maker's danger are introduced. An illustrative model dependent on the outcomes acquired are given.


Keywords: Median ranked set sampling, acceptance sampling plans, logistic distribution, operating characteristic function value, producer's risk, consumer's risk

## Introduction

Ranked Set Sampling (RSS) is a new sampling structure that means to gather more delegate perceptions by spreading over the full scope of estimations in the population. This sampling structure was first proposed by MyIntyre (1952) ${ }^{[9]}$ to assess the mean of field and rummage yields as an option in contrast to the usually utilized Simple Random Sampling(SRS). Generally, the RSS is relevant in any circumstance that expects to expand the accuracy of the factual induction with minimum sample size, and it is utilized for circumstances when the genuine estimations are somewhat hard to test while ranking a little arrangement of test units outwardly is moderately simple and solid.
In this first stage, $m$ independent Simple Random Samples (SRS), every one of size $m$ are drawn from a given part, and afterward a free expense positioning system is utilized to rank the units inside every SRS. In the subsequent stage, the items selected systematically, to such an extent that the thing with the principal rank is chosen from the primary SRS, and afterward in the second SRS the thing with rank two is chosen, still unit with the most extreme position is chosen structure the last SRS (Takahasi and Wakimoto, 1968: Sinha et al., 1996, Chen et al., 2004) ${ }^{[10,11,2]}$. RSS can be utilized in numerous clinical, rural and conservative when the estimation of the testing units is troublesome or costly yet the plan of these units is conceivable without real estimation. Predominantly, a fascinating positioned information inspecting plans proposed by Muttlak (1997) and known by the Median Ranked Set Sampling (MRSS) will be thought of and utilized in this article. The primary benefits of MRSS are the capacity of mistake in positioning decrease and the capacity of expanding the effectiveness of the assessor. The MRSS strategy as given by Muttlak (1997) can be summarized as follows:

Step 1: Select ' $m$ ' random sample "sets" each of size ' $m$ ' from a given population.
Step 2: Rank the items within each set with respect to a variable of interest by cost-free method.
Step 3: If the set size ' $m$ ' is odd, then select for measurement the $\left(\frac{m+1}{2}\right)$ smallest rank (the median) from each set for actual measurement.
Step:4 If the set size ' $m$ ' is even, then select for measurement from the first $m / 2$ samples, the $(\mathrm{m} / 2)^{\mathrm{th}}$ smallest rank: and from the second $\mathrm{m} / 2$ samples select the $\left(\frac{m+1}{2}\right)^{\mathrm{th}}$ smallest for actual measurement.
Step: 5 The cycle may be repeated ' $r$ ' times (i.e. $r$ is number of cycles) to obtain the desired sample size $\mathrm{n}=\mathrm{m}$ *r
. Now, let $X_{11}, X_{12}, \ldots, X_{1 m} ; X_{21}, X_{22}, \ldots, X_{2 m} ; \ldots ; X_{m 1}, X_{m 2}$, ..., $X_{m m}$ be $m$ independent SRS each of size $m$; then among the $m$ samples, select the minimum measurement unit from the first SRS and the second minimum unit from the second SRS, continuing in the same process until we select the maximum measurement unit from the last SRS for actual measurement. The element of the favored MRSS pattern will be inside the shape:
$\left\{X_{[m+1 / 2, m] i j} ; i=1,2, \ldots m, j=1,2, \ldots ., r\right\} m$ is odd
$\left\{X_{[m / 2 ; m] j i}, X_{[m+2 / 2 ; m] k j} ; i=1,2, \ldots, m / 2 ; k=m / 2+1, \ldots . m, j=1,2, \ldots r\right\}$ $m$ is even

## The $i^{\text {th }}$ order statistic is given by,

$\mathrm{F}_{\mathrm{X}(\mathrm{i})}=(\mathrm{F}(\mathrm{x}))^{\mathrm{i}-1}(1-\mathrm{F}(\mathrm{x}))^{\mathrm{n}-\mathrm{I}},-\infty<\mathrm{x}<\infty$
Therefore, Median Ranked Set Sampling is given by
$\mathrm{F}_{\operatorname{MRSS}(\mathrm{x})=}(\mathrm{F}(\mathrm{x}))^{\mathrm{m}}(1-\mathrm{F}(\mathrm{x}))^{\mathrm{m}}$
Most of investigations of positioned insights have been ranked data with assessing the population mean. In any case, none of the past research thought about any of the RSS ideasin the acceptance sampling context, this article could be considered as a new contribution in this practical research area.
Acceptance sampling is an important application in the quality control field, which can be considered as a test procedure, the first time the MRSS statistical procedure is used by the United State military to test bullets before shipping during the World War II. Afterward, utilized in many fields along with clinical and creation.
The technique for the old-style Acceptance Sampling Plan (ASP) in light of an SRS comprises of the resulting steps:

Step: 1 Draw an SRS of size $n$ items from a large lot.
Step: 2 classify each item within the selected sample as defective or non-defective item.
Step: 3 if the number of defective items exceeds the acceptance number (c), then the entire lot is rejected: otherwise, it is accepted.

Therefore, in constructing any acceptance sampling plan we need to find out the minimum sample size(n) to accept a lot and the acceptance number(c), according may call the single sampling plans by $\operatorname{ASP}(\mathrm{n}, \mathrm{c})$. Usually, with every $\operatorname{ASP}(\mathrm{n}, \mathrm{c})$, the problem is to find the unknown parameter n and c that satisfies:
$\mathrm{P}\left(\mathrm{X} \leq \mathrm{c} / \mathrm{n}, \mathrm{p}_{1}\right)=1-\alpha$
$\mathrm{P}\left(\mathrm{X} \leq \mathrm{c} / \mathrm{n}, \mathrm{p}_{2}\right)=\beta$

Where $\alpha$ is the Type I error and $\beta$ is the Type II error. Moreover, $\mathrm{p}_{1}$ is the quality limit for acceptable ( AQL ) and $\mathrm{p}_{2}$ is the per cent defective for lot tolerance (LTPD). The issue that we are introducing in this text is with remembering the MRSS in picking the items from a large lot assuming under the Logistic distributions. The significant idea of the utilization of MRSS in acceptance sampling context is to
bring down the producer danger that ascents while the contraptions chose by means of the ordinary $\operatorname{ASP}(n, c)$ essentially dependent on a SRS techniques.

## Characterization of the Logistic Distribution under MRSS

In this portion, the appropriations could be described fundamentally dependent on the MRSS. The effect of the shape parameter on the distribution structure under MRSS using Logistic distribution.
Characterization of the Logistic Distribution for SRS:
$f(x, \mu, s)=\frac{e^{-(x-\mu) / s}}{s\left[1+e^{-\frac{x-\mu}{s}}\right]^{2}}$
Characterization of the Logistic distribution for MRSS:
$\mathbf{f}_{\text {MRSS }}(\mathbf{x})=\left[\frac{e^{-(x-\mu / s)}}{\left[1+e^{-(x-\mu) / s]^{2}}\right.}\right]^{m}\left[1-\frac{e^{-(x-\mu / s)}}{\left[1+e^{-(x-\mu) / s]^{2}}\right.}\right]^{m}$

## Operating Characteristic (OC) Curve

Related with each inspecting plan there is an OC curve which depicts the exhibition of the sampling plan against great and low quality. The probability that a lot will be acknowledged under a given sampling plan which is indicated by $\mathrm{Pa}(\mathrm{p})$ and a plot of $\mathrm{Pa}(\mathrm{p})$ against given worth of part or process quality p will yield the OC curve. For unique reason designs the OC curve, a curve showing the probability of proceeding to allow the interaction to go on without change as a function of the process quality.
The curve plots the probability of accepting the lot $(\mathrm{Pa})$ versus the lot fraction defective (p)
$\mathrm{Pa}=\mathrm{P}\{\mathrm{d} \leq \mathrm{c}\}=\sum_{i=0}^{c} p^{i} 1-p^{n-i}$
Logistic distribution for MRSS will be
$\mathrm{Pa}=\sum_{i=0}^{c}\left[\frac{e^{-(x-\mu / s)}}{s\left[1+e^{-(x-\mu) / s]^{2}}\right.}\right]^{i}\left[1-\frac{e^{-(x-\mu / s)}}{s\left[1+e^{-(x-\mu) / s]^{2}}\right.}\right]^{(n-i)}$
The given table shows the OC curve values for MRSS using Logistic distribution for $\mathrm{N}=1000, \mathrm{~m}=50, \mathrm{~s}=20, \mathrm{r}=1,2,3,4$, 5,6 and $n=50,100,150,200,250$ and 300.
The following figure-1 shows the OC Curve for the acceptance number $\mathrm{c}=0, \mathrm{~s}=20, \mathrm{~m}=50, \mathrm{r}=1,2,3,4,5,6$ and sample size $n=50,100,150,200,250$ and 300.
It shows the effect of increased sample size on OC curve. We note that each plan uses the same per cent defective which can be allowed for an acceptance lot, the OC curve becomes steeper and lies closer to the origin as the sample size increases.

## Average Sample Number (ASN)

The Average Sample Number (ASN) is characterized as the normal (Expected) number of sample units per lot, which is expected to show up at a choice about the acknowledgment or dismissal of the lot under the acknowledgment sampling plan. The curve drawn between the ASN and the lot quality (p) is known as the ASN curve.

Table 1: The OC Curve Values for Logistic Distribution using MRSS

| N | 1 m | 2 m | 3 m | 4 m | 5 m | 6 m |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P | $\mathrm{C}=0$ |  |  |  |  |  |
| 0.010 | 0.99969 | 0.99385 | 0.99079 | 0.98774 | 0.98469 | 0.98166 |
| 0.015 | 0.99949 | 0.98988 | 0.98486 | 0.97986 | 0.97489 | 0.96994 |
| 0.020 | 0.99916 | 0.98337 | 0.97516 | 0.96702 | 0.95894 | 0.95093 |
| 0.025 | 0.99862 | 0.97273 | 0.95938 | 0.94621 | 0.93322 | 0.92041 |
| 0.030 | 0.99773 | 0.95545 | 0.93392 | 0.91288 | 0.89232 | 0.87221 |
| 0.035 | 0.99626 | 0.92764 | 0.89344 | 0.86051 | 0.82879 | 0.79824 |
| 0.040 | 0.99385 | 0.88357 | 0.83054 | 0.7807 | 0.73384 | 0.6898 |
| 0.045 | 0.98992 | 0.81553 | 0.73647 | 0.66508 | 0.60061 | 0.54239 |
| 0.050 | 0.98351 | 0.71479 | 0.60432 | 0.51092 | 0.43196 | 0.3652 |
| 0.055 | 0.97319 | 0.57557 | 0.43667 | 0.33129 | 0.25134 | 0.19068 |
| P | $\mathrm{C}=1$ |  |  |  |  |  |
| 0.010 | 0.99704 | 0.99397 | 0.99091 | 0.98786 | 0.98481 | 0.98178 |
| 0.015 | 0.99513 | 0.99008 | 0.98506 | 0.98006 | 0.97509 | 0.97014 |
| 0.020 | 0.99198 | 0.9837 | 0.97549 | 0.96734 | 0.95926 | 0.95125 |
| 0.025 | 0.98682 | 0.97327 | 0.95991 | 0.94673 | 0.93373 | 0.92092 |
| 0.030 | 0.97836 | 0.95632 | 0.93478 | 0.91372 | 0.89313 | 0.87301 |
| 0.035 | 0.96459 | 0.92903 | 0.89479 | 0.8618 | 0.83004 | 0.79944 |
| 0.040 | 0.94231 | 0.88576 | 0.8326 | 0.78263 | 0.73566 | 0.69151 |
| 0.045 | 0.90676 | 0.81886 | 0.73948 | 0.6678 | 0.60307 | 0.54461 |
| 0.050 | 0.85115 | 0.71961 | 0.60839 | 0.51437 | 0.43487 | 0.36766 |
| 0.055 | 0.76709 | 0.58197 | 0.44152 | 0.33497 | 0.25413 | 0.1928 |
| P | $\mathrm{C}=2$ |  |  |  |  |  |
| 0.010 | 0.99717 | 0.99409 | 0.99079 | 0.98798 | 0.98494 | 0.9819 |
| 0.015 | 0.99533 | 0.99028 | 0.98526 | 0.98026 | 0.97529 | 0.97034 |
| 0.020 | 0.99232 | 0.98403 | 0.97581 | 0.96766 | 0.95958 | 0.95157 |
| 0.025 | 0.98736 | 0.97381 | 0.96044 | 0.94725 | 0.93425 | 0.92143 |
| 0.030 | 0.97925 | 0.95719 | 0.93563 | 0.91455 | 0.89395 | 0.87381 |
| 0.035 | 0.96604 | 0.93043 | 0.89613 | 0.8631 | 0.83128 | 0.80064 |
| 0.040 | 0.94465 | 0.88796 | 0.83466 | 0.78457 | 0.73749 | 0.69322 |
| 0.045 | 0.91046 | 0.82221 | 0.7425 | 0.67053 | 0.60553 | 0.54683 |
| 0.050 | 0.85688 | 0.72445 | 0.61249 | 0.51783 | 0.4378 | 0.37014 |
| 0.055 | 0.77562 | 0.58843 | 0.44642 | 0.33869 | 0.25695 | 0.19494 |

Table 1 continu..

| n | 1 m | 2 m | 3 m | 4 m | 5 m | 6 m |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| p | $\mathrm{C}=3$ |  |  |  |  |  |
| 0.010 | 0.99729 | 0.99422 | 0.99115 | 0.9881 | 0.98506 | 0.98202 |
| 0.015 | 0.99553 | 0.99048 | 0.98546 | 0.98046 | 0.97548 | 0.97054 |
| 0.020 | 0.99265 | 0.98436 | 0.97614 | 0.96799 | 0.95991 | 0.95189 |
| 0.025 | 0.98791 | 0.97435 | 0.96097 | 0.94778 | 0.93477 | 0.92193 |
| 0.030 | 0.98015 | 0.95807 | 0.93648 | 0.91538 | 0.89476 | 0.8746 |
| 0.035 | 0.96749 | 0.93183 | 0.89748 | 0.8644 | 0.83253 | 0.80185 |
| 0.040 | 0.94699 | 0.89016 | 0.83673 | 0.78652 | 0.73931 | 0.69494 |
| 0.045 | 0.91418 | 0.82557 | 0.74554 | 0.67327 | 0.60801 | 0.54907 |
| 0.050 | 0.86266 | 0.72934 | 0.61662 | 0.52132 | 0.44075 | 0.37263 |
| 0.055 | 0.78423 | 0.59497 | 0.45138 | 0.34245 | 0.2598 | 0.19711 |
| P | $\mathrm{C}=4$ |  |  |  |  |  |
| 0.010 | 0.99741 | 0.99434 | 0.99128 | 0.98822 | 0.98518 | 0.98214 |
| 0.015 | 0.99574 | 0.99069 | 0.98566 | 0.98066 | 0.97568 | 0.97073 |
| 0.020 | 0.99298 | 0.98469 | 0.97647 | 0.96831 | 0.96023 | 0.95221 |
| 0.025 | 0.98846 | 0.97489 | 0.9615 | 0.9483 | 0.93528 | 0.92244 |
| 0.030 | 0.98104 | 0.95894 | 0.93734 | 0.91622 | 0.89558 | 0.8754 |
| 0.035 | 0.96894 | 0.93323 | 0.89883 | 0.8657 | 0.83379 | 0.80305 |
| 0.040 | 0.94934 | 0.89236 | 0.83881 | 0.78847 | 0.74115 | 0.69667 |
| 0.045 | 0.91792 | 0.82894 | 0.74859 | 0.67602 | 0.61049 | 0.55131 |
| 0.050 | 0.86847 | 0.73425 | 0.62077 | 0.52483 | 0.44372 | 0.37515 |
| 0.055 | 0.79294 | 0.60158 | 0.4564 | 0.34625 | 0.26269 | 0.19929 |
| P | $\mathrm{C}=5$ |  |  |  |  |  |
| 0.010 | 0.99753 | 0.99446 | 0.9914 | 0.98835 | 0.9853 | 0.98227 |
| 0.015 | 0.99594 | 0.99089 | 0.98586 | 0.98086 | 0.97588 | 0.97093 |
| 0.020 | 0.99331 | 0.98502 | 0.9768 | 0.96864 | 0.96055 | 0.95253 |
| 0.025 | 0.989 | 0.97543 | 0.96203 | 0.94883 | 0.9358 | 0.92295 |
| 0.030 | 0.98194 | 0.95981 | 0.93819 | 0.91705 | 0.89639 | 0.8762 |
| 0.035 | 0.9704 | 0.93463 | 0.90018 | 0.867 | 0.83504 | 0.80426 |
| 0.040 | 0.95169 | 0.89458 | 0.84089 | 0.79042 | 0.74298 | 0.69839 |
| 0.045 | 0.92167 | 0.83233 | 0.75165 | 0.67878 | 0.61299 | 0.55357 |


| 0.050 | 0.87432 | 0.7392 | 0.62496 | 0.52837 | 0.44671 | 0.37767 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.055 | 0.80175 | 0.60826 | 0.46147 | 0.3501 | 0.26561 | 0.20151 |
| $\mathbf{P}$ | $\mathbf{C}=\mathbf{6}$ |  |  |  |  |  |
| 0.010 | 0.99766 | 0.99459 | 0.99152 | 0.98847 | 0.98542 | 0.98239 |
| 0.015 | 0.99614 | 0.99109 | 0.98606 | 0.98106 | 0.97608 | 0.97113 |
| 0.020 | 0.99365 | 0.98535 | 0.97712 | 0.96896 | 0.96087 | 0.95285 |
| 0.025 | 0.98955 | 0.97596 | 0.96257 | 0.94935 | 0.93632 | 0.92347 |
| 0.030 | 0.98283 | 0.96069 | 0.93905 | 0.91789 | 0.89721 | 0.877 |
| 0.035 | 0.97186 | 0.93604 | 0.90153 | 0.8683 | 0.83629 | 0.80547 |
| 0.040 | 0.95405 | 0.89679 | 0.84297 | 0.79238 | 0.74482 | 0.70012 |
| 0.045 | 0.92544 | 0.83573 | 0.75472 | 0.68156 | 0.61549 | 0.55583 |
| 0.050 | 0.88021 | 0.74418 | 0.62917 | 0.53193 | 0.44972 | 0.38022 |
| 0.055 | 0.81066 | 0.61502 | 0.46659 | 0.35399 | 0.26856 | 0.20375 |



Fig 1: OC Curve for Logistic Distribution using MRSS


Fig 2: ASN Curve for Logistic Distribution using MRSS

In this research, ASN values ( $\mathrm{n}=50,100,150,200,250$ and 300) of single sampling plan under Logistics distribution are same.

## Average Outgoing Quality (AOQ)

A typical strategy, while sampling and testing is nondisastrous, is to 100 per cent review dismissed lots and supplants all defectives with great units. For this situation, all dismissed lots are made awesome and the main deformities left are those in lots that were accepted. AOQ's allude to the drawn out imperfection level for this consolidated LASP (lot acceptance sampling plan) and 100 per cent examination of dismissed lots process. In the event that all parts come in with
a deformity level of precisely p , and the OC curve for the picked ( $\mathrm{n}, \mathrm{c}$ ) LASP demonstrates a probability Pa of tolerating such a lot, for a really long time the AOQ can undoubtedly be demonstrated to be:
$\mathrm{AOQ}=\frac{P a(p)(N-n)}{N}$
Where N is the lot size have given expressions for AOQ to different policies adopted for single sampling attribute plans. In this research, AOQ is approximated as $\mathrm{p} * \mathrm{~Pa}(\mathrm{p})$.
The given table shows the AOQ values for MRSS using Logistic distribution for $\mathrm{N}=1000, \mathrm{~m}=50, \mathrm{~s}=20$, $\mathrm{r}=1,2,3,4,5,6$ and $\mathrm{n}=50,100,150,200,250$ and 300.

Table 2: The AOQ Values for Logistic Distribution using MRSS

| N | 1 m | 2 m | 3 m | 4 m | 5 m | 6 m |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P | $\mathrm{C}=0$ |  |  |  |  |  |
| 0.010 | 0.94971 | 0.89446 | 0.84217 | 0.79019 | 0.73852 | 0.68716 |
| 0.015 | 0.94952 | 0.89089 | 0.83713 | 0.78389 | 0.73117 | 0.67896 |
| 0.020 | 0.9492 | 0.88503 | 0.82888 | 0.77361 | 0.71921 | 0.66565 |
| 0.025 | 0.94869 | 0.87546 | 0.81547 | 0.75697 | 0.69991 | 0.64428 |
| 0.030 | 0.94784 | 0.8599 | 0.79384 | 0.73031 | 0.66924 | 0.61055 |
| 0.035 | 0.94645 | 0.83487 | 0.75943 | 0.68841 | 0.62159 | 0.55877 |
| 0.040 | 0.94416 | 0.79521 | 0.70596 | 0.62456 | 0.55038 | 0.48286 |
| 0.045 | 0.94042 | 0.73397 | 0.626 | 0.53207 | 0.45046 | 0.37967 |
| 0.050 | 0.93434 | 0.64331 | 0.51367 | 0.40874 | 0.32397 | 0.25564 |
| 0.055 | 0.92453 | 0.51802 | 0.37117 | 0.26503 | 0.1885 | 0.13348 |
| P | $\mathrm{C}=1$ |  |  |  |  |  |
| 0.010 | 0.94719 | 0.89457 | 0.84227 | 0.79029 | 0.73861 | 0.68725 |
| 0.015 | 0.94537 | 0.89107 | 0.8373 | 0.78405 | 0.73132 | 0.6791 |
| 0.020 | 0.94238 | 0.88533 | 0.82916 | 0.77387 | 0.71945 | 0.66588 |
| 0.025 | 0.93748 | 0.87594 | 0.81592 | 0.75738 | 0.7003 | 0.64464 |
| 0.030 | 0.92944 | 0.86069 | 0.79456 | 0.73097 | 0.66985 | 0.61111 |
| 0.035 | 0.91636 | 0.83613 | 0.76057 | 0.68944 | 0.62253 | 0.55961 |
| 0.040 | 0.8952 | 0.79718 | 0.70771 | 0.62611 | 0.55175 | 0.48406 |
| 0.045 | 0.86142 | 0.73697 | 0.62856 | 0.53424 | 0.4523 | 0.38123 |
| 0.050 | 0.80859 | 0.64764 | 0.51713 | 0.41149 | 0.32615 | 0.25736 |
| 0.055 | 0.72874 | 0.52377 | 0.37529 | 0.26797 | 0.1906 | 0.13496 |
| P | $\mathrm{C}=2$ |  |  |  |  |  |
| 0.010 | 0.94731 | 0.89468 | 0.84217 | 0.79038 | 0.7387 | 0.68733 |
| 0.015 | 0.94557 | 0.89125 | 0.83747 | 0.78421 | 0.73146 | 0.67924 |
| 0.020 | 0.9427 | 0.88563 | 0.82944 | 0.77413 | 0.71969 | 0.6661 |
| 0.025 | 0.93799 | 0.87643 | 0.81637 | 0.7578 | 0.70069 | 0.645 |
| 0.030 | 0.93029 | 0.86147 | 0.79528 | 0.73164 | 0.67046 | 0.61166 |
| 0.035 | 0.91774 | 0.83738 | 0.76171 | 0.69048 | 0.62346 | 0.56045 |
| 0.040 | 0.89742 | 0.79916 | 0.70947 | 0.62766 | 0.55311 | 0.48526 |
| 0.045 | 0.86494 | 0.73998 | 0.63113 | 0.53642 | 0.45415 | 0.38278 |
| 0.050 | 0.81404 | 0.65201 | 0.52062 | 0.41427 | 0.32835 | 0.2591 |
| 0.055 | 0.73683 | 0.52959 | 0.37946 | 0.27095 | 0.19271 | 0.13646 |

Table 2 continu...

| N | 1 m | 2 m | 3 m | 4 m | 5 m | 6 m |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P | $\mathrm{C}=3$ |  |  |  |  |  |
| 0.010 | 0.94742 | 0.8948 | 0.84248 | 0.79048 | 0.73879 | 0.68742 |
| 0.015 | 0.94576 | 0.89144 | 0.83764 | 0.78437 | 0.73161 | 0.67938 |
| 0.020 | 0.94302 | 0.88592 | 0.82972 | 0.77439 | 0.71993 | 0.66632 |
| 0.025 | 0.93851 | 0.87691 | 0.81683 | 0.75822 | 0.70108 | 0.64535 |
| 0.030 | 0.93114 | 0.86226 | 0.79601 | 0.73231 | 0.67107 | 0.61222 |
| 0.035 | 0.91911 | 0.83864 | 0.76286 | 0.69152 | 0.6244 | 0.56129 |
| 0.040 | 0.89964 | 0.80114 | 0.71122 | 0.62921 | 0.55448 | 0.48646 |
| 0.045 | 0.86847 | 0.74301 | 0.63371 | 0.53862 | 0.456 | 0.38435 |
| 0.050 | 0.81952 | 0.6564 | 0.52413 | 0.41706 | 0.33056 | 0.26084 |
| 0.055 | 0.74502 | 0.53547 | 0.38368 | 0.27396 | 0.19485 | 0.13797 |
| P | $\mathrm{C}=4$ |  |  |  |  |  |
| 0.010 | 0.94754 | 0.89491 | 0.84259 | 0.79058 | 0.73888 | 0.6875 |
| 0.015 | 0.94595 | 0.89162 | 0.83781 | 0.78453 | 0.73176 | 0.67951 |
| 0.020 | 0.94333 | 0.88622 | 0.83 | 0.77465 | 0.72017 | 0.66655 |
| 0.025 | 0.93903 | 0.8774 | 0.81728 | 0.75864 | 0.70146 | 0.64571 |
| 0.030 | 0.93199 | 0.86305 | 0.79674 | 0.73297 | 0.67168 | 0.61278 |
| 0.035 | 0.9205 | 0.8399 | 0.764 | 0.69256 | 0.62534 | 0.56214 |
| 0.040 | 0.90187 | 0.80313 | 0.71299 | 0.63077 | 0.55586 | 0.48767 |
| 0.045 | 0.87202 | 0.74605 | 0.6363 | 0.54082 | 0.45787 | 0.38592 |
| 0.050 | 0.82505 | 0.66082 | 0.52766 | 0.41987 | 0.33279 | 0.2626 |
| 0.055 | 0.7533 | 0.54142 | 0.38794 | 0.277 | 0.19702 | 0.13951 |
| P | $\mathrm{C}=5$ |  |  |  |  |  |
| 0.010 | 0.94766 | 0.89502 | 0.84269 | 0.79068 | 0.73898 | 0.68759 |
| 0.015 | 0.94614 | 0.8918 | 0.83798 | 0.78469 | 0.73191 | 0.67965 |
| 0.020 | 0.94365 | 0.88652 | 0.83028 | 0.77491 | 0.72041 | 0.66677 |
| 0.025 | 0.93955 | 0.87788 | 0.81773 | 0.75906 | 0.70185 | 0.64607 |
| 0.030 | 0.93284 | 0.86383 | 0.79746 | 0.73364 | 0.67229 | 0.61334 |
| 0.035 | 0.92188 | 0.84117 | 0.76515 | 0.6936 | 0.62628 | 0.56298 |
| 0.040 | 0.90411 | 0.80512 | 0.71475 | 0.63234 | 0.55724 | 0.48887 |
| 0.045 | 0.87559 | 0.74909 | 0.6389 | 0.54303 | 0.45974 | 0.3875 |


| 0.050 | 0.83061 | 0.66528 | 0.53121 | 0.4227 | 0.33503 | 0.26437 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.055 | 0.76167 | 0.54744 | 0.39225 | 0.28008 | 0.19921 | 0.14106 |
| $\mathbf{P}$ | $\mathbf{C = 6}$ |  |  |  |  |  |
| 0.010 | 0.94778 | 0.89513 | 0.84279 | 0.79077 | 0.73907 | 0.68767 |
| 0.015 | 0.94633 | 0.89198 | 0.83815 | 0.78485 | 0.73206 | 0.67979 |
| 0.020 | 0.94397 | 0.88682 | 0.83055 | 0.77517 | 0.72065 | 0.66699 |
| 0.025 | 0.94007 | 0.87837 | 0.81818 | 0.75948 | 0.70224 | 0.64643 |
| 0.030 | 0.93369 | 0.86462 | 0.79819 | 0.73431 | 0.67291 | 0.6139 |
| 0.035 | 0.92327 | 0.84243 | 0.7663 | 0.69464 | 0.62722 | 0.56383 |
| 0.040 | 0.90635 | 0.80711 | 0.71653 | 0.6339 | 0.55862 | 0.49009 |
| 0.045 | 0.87916 | 0.75216 | 0.64151 | 0.54525 | 0.46162 | 0.38908 |
| 0.050 | 0.8362 | 0.66976 | 0.53479 | 0.42554 | 0.33729 | 0.26615 |
| 0.055 | 0.77013 | 0.55352 | 0.39661 | 0.28319 | 0.20142 | 0.14262 |

The following figure-3 shows the AOQ Curve for the sample size $\mathrm{n}=50,100,150,200,250$ and 300. acceptance number $\mathrm{c}=0, \mathrm{~s}=20, \mathrm{~m}=50, \mathrm{r}=1,2,3,4,5,6$ and


Fig 3: AOQ Curve for Logistic Distribution using MRSS

For the acceptance sampling plan in which rectification is not done, the AOQ is the same as the incoming quality. Therefore when the lot is either accepted or rejected, the AOQ is the same as the quality of the submitted lot.

## Average Total Inspection (ATI)

At the point when dismissed lots are 100 per cent investigated, it is not difficult to work out the ATI if lots come reliably with a deformity level of ' p '. For a $\operatorname{LASP}$ ( $n, ~ c$ )
with a probability Pa of tolerating a lot with deformity level p , one can have
$\mathrm{ATI}=\mathrm{n}+(1-\mathrm{Pa})(\mathrm{N}-\mathrm{n})$
Where N is the lot size, n is the sample size.
Table 3 shows the ATI values for MRSS using Logistic distribution for $\mathrm{N}=1000, \mathrm{~m}=50, \mathrm{~s}=20$,
$\mathrm{r}=1,2,3,4,5,6$ and $\mathrm{n}=50,100,150,200,250$ and 300.

Table 3: The ATI Values for Logistic Distribution using MRSS

| n | 1 m | 2 m | 3 m | 4 m | 5 m | 6 m |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P | $\mathrm{C}=0$ |  |  |  |  |  |
| 0.010 | 50.29298 | 105.536 | 157.8306 | 209.8115 | 261.4802 | 312.838 |
| 0.015 | 50.48292 | 109.1087 | 162.8713 | 216.1114 | 268.8327 | 321.0393 |
| 0.020 | 50.79587 | 114.9674 | 171.1155 | 226.3875 | 280.7943 | 334.3464 |
| 0.025 | 51.31125 | 124.5411 | 184.5285 | 243.0338 | 300.0865 | 355.7154 |
| 0.030 | 52.15942 | 140.0954 | 206.1644 | 269.6929 | 330.7619 | 389.4499 |
| 0.035 | 53.55356 | 165.1273 | 240.5738 | 311.5927 | 378.4077 | 441.2323 |
| 0.040 | 55.84065 | 204.7866 | 294.039 | 375.4426 | 449.618 | 517.1396 |
| 0.045 | 59.58055 | 266.0267 | 373.9983 | 467.9341 | 549.5407 | 620.3257 |
| 0.050 | 65.66381 | 356.6896 | 486.3279 | 591.261 | 676.0288 | 744.358 |
| 0.055 | 75.47357 | 481.9833 | 628.8317 | 734.9715 | 811.4987 | 866.5244 |
| P | $\mathrm{C}=1$ |  |  |  |  |  |
| 0.010 | 52.80941 | 105.4256 | 157.7267 | 209.714 | 261.389 | 312.7532 |
| 0.015 | 54.6273 | 108.9275 | 162.701 | 215.9519 | 268.684 | 320.9012 |
| 0.020 | 57.61657 | 114.6705 | 170.8374 | 226.128 | 280.553 | 334.1231 |
| 0.025 | 62.52356 | 124.0569 | 184.0775 | 242.6152 | 299.6994 | 355.359 |
| 0.030 | 70.55578 | 139.3113 | 205.4405 | 269.027 | 330.1516 | 388.8931 |
| 0.035 | 83.64253 | 163.8721 | 239.4321 | 310.5577 | 377.4732 | 440.3922 |
| 0.040 | 104.8014 | 202.8155 | 292.2891 | 373.8945 | 448.2537 | 515.9427 |
| 0.045 | 138.5825 | 263.0272 | 371.44 | 465.7596 | 547.6997 | 618.774 |
| 0.050 | 191.4087 | 352.355 | 482.8668 | 588.5069 | 673.8459 | 742.6355 |


| 0.055 | 271.2607 | 476.2286 | 624.7084 | 732.0273 | 809.4046 | 865.0416 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{P}$ | $\mathbf{C = 2}$ |  |  |  |  |  |  |
| 0.010 | 52.69252 | 105.3152 | 157.8306 | 209.6165 | 261.2979 | 312.6684 |  |
| 0.015 | 54.43495 | 108.7462 | 162.5306 | 215.7923 | 268.5352 | 320.763 |  |
| 0.020 | 57.30043 | 114.3735 | 170.5592 | 225.8684 | 280.3117 | 333.8997 |  |
| 0.025 | 62.00505 | 123.5724 | 183.6262 | 242.1963 | 299.3121 | 35.0025 |  |
| 0.030 | 69.70824 | 138.5264 | 204.716 | 268.3604 | 329.5408 | 388.3359 |  |
| 0.035 | 82.26484 | 162.6151 | 238.2886 | 309.5212 | 376.5372 | 439.5509 |  |
| 0.040 | 102.5825 | 200.8394 | 290.5349 | 372.3425 | 446.8861 | 514.7429 |  |
| 0.045 | 135.062 | 260.0153 | 368.8712 | 463.5763 | 545.8513 | 617.216 |  |
| 0.050 | 185.9604 | 347.9912 | 479.3823 | 585.7343 | 671.6483 | 740.9014 |  |
| 0.055 | 263.1651 | 470.4101 | 620.5393 | 729.0504 | 807.2873 | 863.5424 |  |

Table 3 Continu...

| N | 1 m | 2 m | 3 m | 4 m | 5 m | 6 m |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P | C=3 |  |  |  |  |  |
| 0.010 | 52.57561 | 105.2048 | 157.5188 | 209.5189 | 261.2067 | 312.5836 |
| 0.015 | 54.24255 | 108.5648 | 162.3602 | 215.6328 | 268.3863 | 320.6248 |
| 0.020 | 56.98419 | 114.0764 | 170.281 | 225.6087 | 280.0703 | 333.6763 |
| 0.025 | 61.48626 | 123.0877 | 183.1747 | 241.7771 | 298.9245 | 354.6457 |
| 0.030 | 68.85992 | 137.7409 | 203.9908 | 267.6933 | 328.9294 | 387.7781 |
| 0.035 | 80.88508 | 161.3561 | 237.1434 | 308.4831 | 375.5999 | 438.7083 |
| 0.040 | 100.358 | 198.8585 | 288.7763 | 370.7867 | 445.5151 | 513.54 |
| 0.045 | 131.5272 | 256.9912 | 366.2919 | 461.3841 | 543.9953 | 615.6517 |
| 0.050 | 180.4755 | 343.598 | 475.8744 | 582.943 | 669.4359 | 739.1556 |
| 0.055 | 254.9796 | 464.5268 | 616.3239 | 726.0404 | 805.1464 | 862.0265 |
| P | $\mathrm{C}=4$ |  |  |  |  |  |
| 0.010 | 52.45869 | 105.0944 | 157.4148 | 209.4214 | 261.1156 | 312.4988 |
| 0.015 | 54.05012 | 108.3834 | 162.1898 | 215.4732 | 268.2375 | 320.4866 |
| 0.020 | 56.66785 | 113.7793 | 170.0027 | 225.3489 | 279.8287 | 333.4528 |
| 0.025 | 60.96719 | 122.6027 | 182.7229 | 241.3578 | 298.5368 | 354.2888 |
| 0.030 | 68.01084 | 136.9546 | 203.2649 | 267.0255 | 328.3175 | 387.2198 |
| 0.035 | 79.50325 | 160.0952 | 235.9965 | 307.4434 | 374.6611 | 437.8644 |
| 0.040 | 98.12801 | 196.8727 | 287.0133 | 369.2271 | 444.1406 | 512.3342 |
| 0.045 | 127.978 | 253.9547 | 363.7021 | 459.1829 | 542.1317 | 614.081 |
| 0.050 | 174.9536 | 339.1752 | 472.3429 | 580.1329 | 667.2085 | 737.398 |
| 0.055 | 246.7032 | 458.5783 | 612.0616 | 722.997 | 802.9818 | 860.4937 |
| P | C=5 |  |  |  |  |  |
| 0.010 | 52.34175 | 104.9839 | 157.3108 | 209.3238 | 261.0244 | 312.4139 |
| 0.015 | 53.85765 | 108.202 | 162.0193 | 215.3136 | 268.0886 | 320.3483 |
| 0.020 | 56.35139 | 113.482 | 169.7242 | 225.089 | 279.5872 | 333.2292 |
| 0.025 | 60.44782 | 122.1174 | 182.2709 | 240.9382 | 298.1488 | 353.9317 |
| 0.030 | 67.16097 | 136.1676 | 202.5384 | 266.3571 | 327.705 | 386.6611 |
| 0.035 | 78.11934 | 158.8325 | 234.8479 | 306.4022 | 373.721 | 437.0193 |
| 0.040 | 95.89249 | 194.8819 | 285.246 | 367.6635 | 442.7628 | 511.1254 |
| 0.045 | 124.4142 | 250.9057 | 361.1017 | 456.9727 | 540.2605 | 612.5038 |
| 0.050 | 169.3944 | 334.7226 | 468.7876 | 577.3038 | 664.9662 | 735.6286 |
| 0.055 | 238.3348 | 452.5636 | 607.752 | 719.9198 | 800.7931 | 858.9439 |
| P | (边 C=6 |  |  |  |  |  |
| 0.010 | 52.2248 | 104.8735 | 157.2068 | 209.2262 | 260.9332 | 312.3291 |
| 0.015 | 53.66514 | 108.0206 | 161.8488 | 215.1539 | 267.9397 | 320.21 |
| 0.020 | 56.03484 | 113.1846 | 169.4457 | 224.8291 | 279.3455 | 333.0055 |
| 0.025 | 59.92817 | 121.6319 | 181.8186 | 240.5183 | 297.7606 | 353.5743 |
| 0.030 | 66.31033 | 135.3799 | 201.8112 | 265.6881 | 327.0919 | 386.1018 |
| 0.035 | 76.73335 | 157.5679 | 233.6975 | 305.3594 | 372.7794 | 436.1729 |
| 0.040 | 93.65143 | 192.8862 | 283.4743 | 366.0961 | 441.3816 | 509.9136 |
| 0.045 | 120.8359 | 247.8444 | 358.4906 | 454.7535 | 538.3817 | 610.9202 |
| 0.050 | 163.7979 | 330.24 | 465.2083 | 574.4557 | 662.7088 | 733.8473 |
| 0.055 | 229.8735 | 446.4822 | 603.3946 | 716.8084 | 798.5801 | 857.377 |

The following figure-4 shows the ATI Curve for the sample size $\mathrm{n}=50,100,150,200,250$ and 300.
acceptance number $\mathrm{c}=0, \mathrm{~s}=20, \mathrm{~m}=50, \mathrm{r}=1,2,3,4,5,6$ and


Fig 4: ATI Curve for Logistic Distribution using MRSS

The curve drawn between ATI and the lot quality (p) is known as ATI curve. A typical ATI curve for a single sample plan is shown for $\mathrm{N}=1000, \mathrm{n}=50,100,150,200,250$ and 300.

## Illustration

A manufacturer of Furniture Company produces wooden tables in lots (N) of 1000 by using MRSS method, distributed by Logistic distribution. Then, the scale parameter (s) is 20, sample set size (m) is 50 and the cycle size (r) is 6 . The quality of incoming lot is 0.03 and acceptance numbers are 0 and 1.

## Explanation

It is given, sample size of wooden tables $\mathrm{m}=50$ and sample cycle size $r=6$ (specified by the producer). Hence, $n=m * r$ $(300=50 * 6)$. For a fixed lot quality $p=0.03$, the value of the parameter (s) is 20. Then $[m, r]_{i j}$ is the $(\mathrm{m}, \mathrm{r})^{t h}$ judgment order statistics of the $i^{\text {th }}$ random sample of size $m$ in the $j^{t h}$ cycle. In a sample of $n=300$ specimens selected from a lot of an wooden table manufacturing company, if $\mathrm{X} \leq \mathrm{c}$, the lot is accepted, otherwise reject the lot and inform the management for further action. If X represents the number of defective wooden tables in the sample, if $\mathrm{X}=0$ the probability of accepting the lot $\mathrm{Pa}(\mathrm{p})$ is 0.87221 , ASN is 300 , AOQ is 0.61055 , ATI is 389 ( 389.44 is equivalent to 389 ). If $\mathrm{X}=1$ the probability of accepting the lot $\mathrm{Pa}(\mathrm{p})$ is $0.87301, \mathrm{ASN}$ is 300 , AOQ is 0.6111 , ATI is 389 .

## Conclusion

Construction of Acceptance Sampling Plans for the Median Ranked Set Sampling using Logistic Distribution makes to optimize the designing process in the easy way in the determination of the parameters in the inspection quality control. Objectives of minimizing the AOQ, ASN and ATI are concerned in the optimization process.
An application has been considered in the Sampling such that AOQ, ASN or ATI is minimized subject to the probabilistic constraints considered by Guenther (1969). It was found to work very well in the process of the Operating Characteristic curve is drawn for the chosen sampling and which is more discriminating than the existing.
In this paper, another MRSS technique is recommended for considering Operating Characteristic Curve, Average Sample Number, Average Outgoing Quality and Average Total Inspection. It is more effective than basic arbitrary testing on the grounds that fewer samples should be gathered and
estimated. The output of the results shows that sample size amounts decrease as indeterminacy amounts increase. It has been advised to use the proposed sampling plans, because it is cost-effective. The made arrangement may be utilized to assess huge information examination beginning with wellbeing exploration, biology and different regions that could be extended.
This study can be extended further for the various parameters such as AQL, LQL, IQL, AOQL, MAPD and MAAOQL. Further it can be extended to Double Sampling Plan, Multistage Sampling Plan, other Special Purpose Plans as Chain Sampling, Skip Plot Sampling Plans as well.

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